

# **ME 321: FLUID MECHANICS-I**

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Lecture-06

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Fluid dynamics

Conservation of Mass
(Continuity Equation)

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#### Recap



Reynolds transport theorem (RTT) for a fixed, nondeforming control volume (CV)

$$\frac{d}{dt} \left( B_{\text{syst}} \right) = \frac{d}{dt} \left( \int_{\text{CV}} \beta \rho d \mathcal{V} \right) + \int_{\text{CS}} \beta \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA$$

This relation permits to change from a system approach to control volume (CV) approach.

where

$$B_{syst}$$
 = any property of fluid (mass, momentum, enthalpy, etc.)

 $\beta$  = intensive property of fluid (per unit mass basis)

 $\rho$  = density of fluid

 $d\mathcal{V} = \text{elemental volume}$ 

 $(\vec{\mathbf{V}} \cdot \hat{\mathbf{n}}) dA$  = elemental volume flux

= volume integral over the control volume (CV)

= surface integral over the control surface (CS)

Similar expression adopted by other books:

$$\frac{D}{Dt} \left( B_{\text{syst}} \right) = \frac{\partial}{\partial t} \left( \int_{CV} \beta \rho d\Psi \right) + \int_{CS} \beta \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA$$

#### **Conservation of Mass**

Reynolds transport theorem (RTT) with B = mass and so,  $\beta$  = 1; accordingly

$$\Rightarrow \frac{d}{dt} (m_{\text{syst}}) = \frac{d}{dt} (\int_{\text{CV}} \rho d \mathcal{V}) + \int_{\text{CS}} \rho (\vec{\mathbf{V}} \cdot \hat{\mathbf{n}}) dA$$

$$\Rightarrow \frac{d}{dt} \int_{CV} \rho d\Psi + \int_{CS} \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA = 0$$

Control volume expression for conservation of mass, commonly known as <u>continuity equation</u>.

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#### **Conservation of Mass**

For steady flow i.e. 
$$\frac{d}{dt}()=0$$

$$\frac{d}{dt} \int_{CV} \rho \, d\mathcal{V} + \int_{CS} \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA = 0$$

$$\Rightarrow \int_{\rm CS} \rho\left(\vec{\mathbf{V}} \cdot \hat{\mathbf{n}}\right) dA = 0 \qquad (ii)$$



The integrand in the mass flow rate integral represents the product of the component of velocity, **V** perpendicular to the small portion of the control surface and the differential area, dA.

As shown in figure (dot product)

 $(\vec{\mathbf{V}} \cdot \hat{\mathbf{n}}) = + ve$ ; +ve for flow out from the control volume  $(\vec{\mathbf{V}} \cdot \hat{\mathbf{n}}) = -ve$ ; -ve for flow in to the control volume

# Equation (ii) states that in steady flow, the mass flows entering and leaving the control volume (CV) must balance exactly.



#### **Conservation of Mass**

When all of the differential quantities are summed over the entire control surfaces;

$$\int_{CS} \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA = 0 = \sum \left( \rho AV \right)_{\text{out}} - \sum \left( \rho AV \right)_{\text{in}} = 0$$

$$= \sum \dot{m}_{\text{out}} - \sum \dot{m}_{\text{in}} = 0$$

$$\Rightarrow \sum \dot{m}_{\text{in}} = \sum \dot{m}_{\text{out}}$$
Mass continuity equation

For incompressible flows, ( $\rho$  =constant through the flow system)

$$\Rightarrow \sum (AV)_{in} = \sum (AV)_{out}$$
$$\Rightarrow \sum Q_{in} = \sum Q_{out}$$
volume continuity equation



Control

surface

#### **Problem**



What is the requirement of velocity ratio,  $V_A : V_B$  to keep the water level same in the tank?



Ans: rising, 4.



#### **Problem**



A worker is performing maintenance in a small rectangular tank with a height of 3 m and square base 1.8 m by 1.8 m. Fresh air enters though a 200 mm diameter hose and exists through a 100 mm diameter port on the tank wall. Assume the flow to be steady and incompressible.

- (a) Determine the exchange rate needed for the ventilation safety of the worker inside the tank. A complete change of air every 3 minutes (Air Change per Hour, ACH = 20) has been generally accepted by industry as per ventilation requirement.
- (b) Determine the velocity of the air entering and existing the tank at this exchange rate.

Ans: (a) 3.24 m<sup>3</sup>/min (120 cfm) (b) 1.72 m/s, 6.88 m/s



The tank in Fig. is being filled with water by two one-dimensional inlets. Air is trapped at the top of the tank. The water height is h.

- (a) Find an expression for the change in water height dh/dt.
- (b) Compute dh/dt if  $D_1 = 25$  mm,  $D_2 = 75$  mm,  $V_1 = 0.75$  m/s,  $V_2 = 0.60$  m/s, and  $A_t = 0.2$  m<sup>2</sup>.



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#### **Solution:**

General Continuity Equation in integral form applied to the shown control volume

$$\frac{d}{dt} \int_{CV} \rho \, d\mathcal{V} + \int_{CS} \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA = 0 \qquad \qquad \text{Unsteady, } \frac{d}{dt} \int_{CV} \rho \, d\mathcal{V} \neq 0$$





$$\frac{d}{dt}\left(\int_{CV}\rho d\Psi\right) - \rho_1 A_1 V_1 - \rho_2 A_2 V_2 = 0$$

Now,

$$\frac{d}{dt}\left(\int_{CV} \rho d\mathcal{V}\right) = \frac{d}{dt}(m_{CV}) = \frac{d}{dt}(\rho_w A_t h) + \frac{d}{dt}[\rho_a A_t(H-h)]$$
 of air mass with time)

Tank area  $A_t$   $\rho_a$  H h  $\rho_w$   $\rho_w$   $\rho_w$  $\rho_w$ 

 $\Rightarrow \frac{d}{dt} \left( \int_{CV} \rho d\Psi \right) = \rho_{W} A_{t} \frac{dh}{dt}$ 

Fixed CS

Thus,

$$\frac{dh}{dt} = \frac{\rho_1 A_1 V_1 + \rho_2 A_2 V_2}{\rho_w A_t}$$
$$\Rightarrow \frac{dh}{dt} = \frac{A_1 V_1 + A_2 V}{A_t}$$
$$\Rightarrow \frac{dh}{dt} = \frac{Q_1 + Q_2}{A_t}$$
Ans. (a)



= 0

(air is trapped, no change







$$\Rightarrow \frac{dh}{dt} = \frac{Q_1 + Q_2}{A_t}$$

$$\Rightarrow \frac{dh}{dt} = \frac{\pi/4D_1^2 V_1 + \pi/4D_2^2 V_2}{A_t}$$
$$\Rightarrow \frac{dh}{dt} = 0.015 \text{ m/s} \qquad \text{Ans. (b)}$$

A 1.5 m high, 1 m diameter cylindrical water tank whose top is open to the atmosphere is initially filled with water. Now, the discharge plug near the bottom of the tank is pulled out, and a water jet whose diameter is 0.01 m streams out (Fig.). The average velocity of the jet is given by:

$$V_{jet} = \sqrt{2gh}$$
 (m/s)

where *h* is the height of water in the tank measured from the center of the hole and g is the gravitational acceleration. Determine

- (i) How long it will take for the water level in the tank to drop to 0.75 m from the bottom?
- (ii) How long it will take to empty the tank?

#### Solution:

General Continuity Equation in integral form applied to the shown control volume

$$\frac{d}{dt} \int_{CV} \rho \, d\mathcal{V} + \int_{CS} \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA = 0 \qquad \qquad \text{Unsteady, } \frac{d}{dt} \int_{CV} \rho \, d\mathcal{V} \neq 0$$





$$\frac{d}{dt} \int_{CV} \rho \, d\mathcal{V} + \int_{CS} \rho \left( \vec{\mathbf{V}} \cdot \hat{\mathbf{n}} \right) dA = 0$$

 $\Rightarrow \frac{d}{dt} (m_{\rm CV}) + \rho A_{\rm jet} V_{\rm jet} = 0$ 

No inflow; only out flow through the hole (+ve)

$$m_{\rm CV} = \rho \Psi = \rho \left(\frac{\pi}{4} D_{\rm tank}^2 \times h\right) \qquad \qquad h = h(t); \quad m_{\rm CV} = f(t)$$
$$\rho A_{\rm jet} V_{\rm jet} = \rho \left(\frac{\pi}{4} D_{\rm jet}^2\right) \sqrt{2gh} \qquad \qquad V_{\rm jet} = \sqrt{2gh} = f(t)$$



Then,

$$\Rightarrow \frac{d}{dt} \left\{ \rho \left( \frac{\pi}{4} D_{\text{tank}}^2 \times h \right) \right\} + \rho \left( \frac{\pi}{4} D_{\text{jet}}^2 \right) \sqrt{2gh} = 0$$
$$\Rightarrow \frac{d}{dt} \left\{ \left( D_{\text{tank}}^2 \times h \right) \right\} = -\left( D_{\text{jet}}^2 \right) \sqrt{2gh}$$
$$\boxed{\Rightarrow \frac{dh}{dt} = -\left( \frac{D_{\text{jet}}^2}{D_{\text{tank}}^2} \right) \sqrt{2gh}}$$

Unsteady,  $\frac{\partial}{\partial t} \int_{CV} \rho \, d\mathcal{V} \neq 0$ 



$$\Rightarrow dt = -\frac{1}{\sqrt{2g}} \frac{D_{\text{tank}}^2}{D_{\text{jet}}^2} \frac{dh}{\sqrt{h}}$$

Now, integrating from t = 0 at which  $h = h_0$  to t = t at which  $h = h_t$ 

$$\int_{0}^{t} dt = -\frac{1}{\sqrt{2g}} \frac{D_{\text{tank}}^{2}}{D_{\text{jet}}^{2}} \int_{h_{0}}^{h_{t}} \frac{dh}{\sqrt{h}}$$
$$\Rightarrow t = -\frac{1}{\sqrt{2g}} \frac{D_{\text{tank}}^{2}}{D_{\text{jet}}^{2}} \left[ \frac{h^{-\frac{1}{2}+1}}{-\frac{1}{2}+1} \right]_{h_{0}}^{h_{t}}$$

$$\Rightarrow t = -\frac{1}{\sqrt{g/2}} \frac{D_{\text{tank}}^2}{D_{\text{jet}}^2} \left| \sqrt{h} \right|_{h_0}^{h_t}$$

$$\Rightarrow t = \frac{\sqrt{h_0} - \sqrt{h_t}}{\sqrt{g/2}} \frac{D_{\text{tank}}^2}{D_{\text{jet}}^2}$$

Time required to reduce the water height from  $h_0$  to  $h_t$ 







Time required for the water level in the tank to drop to 0.75 m from the bottom:

$$t = \frac{\sqrt{h_0} - \sqrt{h_t}}{\sqrt{g/2}} \frac{D_{\text{tank}}^2}{D_{\text{jet}}^2}$$

$$\therefore t_{h_t=0.75} = \frac{\sqrt{1.5} - \sqrt{0.75}}{\sqrt{g/2}} \frac{1^2}{0.01^2} = 1619.7 \,\mathrm{s} = 27 \,\mathrm{min} \, \left( -\frac{1}{2} + \frac{1}{2} +$$



Time required to empty the water tank:

$$\therefore t_{h_t=0} = \frac{\sqrt{1.5} - \sqrt{0}}{\sqrt{g/2}} \frac{1^2}{0.01^2} = 5530 \text{ s} = 92 \text{ min}$$

Time requirement is **NOT linear (rather non-linear)** (AN UNSTEADY PROBLEM)

Homework:

Plot the water height, *h* versus time, *t* 



Methane escapes through a small  $(10^{-7} \text{ m}^2)$  hole in a 10 m<sup>3</sup> tank. The methane escapes so slowly that the temperature in the tank remains constant at 23°C. The mass flow rate of methane through the hole is given by  $\dot{m} = 0.66 pA/\sqrt{RT}$ , where *p* is the pressure in the tank, *A* is the area of the hole, *R* is the gas constant, and *T* is the temperature in the tank. Calculate the time required for the absolute pressure in the tank to decrease from 500 to 400 kPa.





• There is no mass inflow:

$$\sum_{\rm cs} \dot{m}_i = 0$$

• Mass out flow rate is

$$\sum_{\rm cs} \dot{m}_o = 0.66 \frac{pA}{\sqrt{RT}}$$

Substituting terms into the continuity equation gives

$$\Psi \frac{d\rho}{dt} = -0.66 \frac{pA}{\sqrt{RT}}$$

3. Equation for elapsed time:

• Use ideal gas law for  $\rho$ :

$$\Psi \frac{\mathrm{d}}{\mathrm{d}t} \left(\frac{p}{RT}\right) = -0.66 \frac{pA}{\sqrt{RT}}$$

• Because R and T are constant,

$$\frac{\mathrm{d}p}{\mathrm{d}t} = -0.66 \,\frac{pA\sqrt{RT}}{\Psi}$$

• Next, separate variables:

$$\frac{dp}{p} = -0.66 \frac{A\sqrt{RT}dt}{V}$$

• Integrating the equation and substituting limits for initial and final pressure gives

$$t = \frac{1.52 \,\forall}{A \,\sqrt{RT}} \,\ln\frac{P_0}{P_f}$$

4. Elapsed time:

$$t = \frac{1.52 \,(10 \,\mathrm{m}^3)}{(10^{-7} \,\mathrm{m}^2) \left(518 \,\frac{\mathrm{J}}{\mathrm{kg} \cdot \mathrm{K}} \times 300 \,\mathrm{K}\right)^{1/2}} \,\ln\frac{500}{400} = \boxed{8.6 \times 10^4 \,\mathrm{s}}$$

#### **Review the Solution and the Process**

- 1. *Discussion*. The time corresponds to approximately one day.
- 2. *Knowledge.* Because the ideal gas law is used, the pressure and temperature have to be in absolute values.

